EE 505

Lecture 25

ADC Design

Performance Limitations

(consider amplifier, ADC and DAC issues)

- ADC
 - Break Points (offsets)
- DAC
 - DAC Levels (offsets)
 - Out-range (over or under range)
- Amplifier
 - Offset voltages
 - Settling Time
 - Nonlinearity (primarily open loop)
 - Open-loop
 - Out-range
 - Gain Errors
 - Inadequate open loop gain
 - Component mismatch
 - Power Dissipation
 - kT/C switching noise



Review from last lecture How Much Gain?

Depends upon how much of the overall error budget is allocated to the effect noninfinite gain has on required performance parameters

If require n ENOB, can $\frac{1}{2}$ LSB be allocated to effects of op amp gain error?

e.g. If INL specification of a 12-bit ADC is $\frac{1}{2}$ LSB, can $\frac{1}{2}$ LSB be allocated to the noninfinite gain error?

Sources that may contribute to INL errors in pipelined ADC:

Finite Op Amp Gain Capacitor Missmatch Incomplete amplifier settling Amplifier nonlinearity Input S/H error Parasitic capacitance nonlinearity Offset voltage (in ADC, DAC, summer) DAC errors ADC nonlinaritry Review from last lecture Error Budgeting

Sources that may contribute to INL errors in pipelined ADC:

Finite Op Amp Gain Capacitor Missmatch Incomplete amplifier settling Amplifier nonlinearity Input S/H error Parasitic capacitance nonlinearity Offset voltage (in ADC, DAC, summer) DAC errors ADC nonlinaritry

If entire error budget (e.g. ½ LSB) is allocated to the Finite Op Amp Gain, what error budget must be allocated to all remaining contributors?

What will happen if each error source is allocated an error budget of (e.g. ½ LSB)?

How should the error sources contribution to overall error budget be allocated?

 $\sum_{i=1}^{m} e_i = \frac{1}{2} LSB \quad \text{(maybe a little bit overly conservative)}$



 C_L is the parallel combination of any interconnect capacitance, the capacitance of the β network and the sampling capacitance of the following stage

For MOS implementation (with ref SE op amp or telescopic cascade op amp)

$$GB = \frac{2I_{DQ}}{V_{EB}C_{L}} = \left(\frac{1}{(V_{DD}-V_{SS})}\frac{P}{C_{L}}\right)\frac{1}{V_{EB}}$$
$$P = V_{SUP} \bullet GB \bullet C_{L} \bullet V_{EB}$$

For convenience, define

$$V_{SUP} = V_{DD} - V_{SS}$$

- Keep V_{EB} small, C_L as small as possible, GB as small as possible
- At high speeds, diffusion parasitics will cause P to increase more rapidly than GB
- Total amplifier power is sum of power in each stage

Settling Time

Conventional Approach: Assume want to make at most ½ LSB error in settling for worst-case step in each stage



Note: GB requirements drop from stage to stage



Interleaving can dramatically reduce power requirements (e.g. two interleaved stages reduce GB requirements a factor of 2 on each stage thereby maintaining power requirements on linear slope region) for high speed data converters but introduces some calibration challenges



GB_{LIM} strongly technology dependent

What do we do if system requirements are in the respective scenarios?



Capacitor sizing strategies



Size of C affects both the noise $(\sqrt{\frac{kT}{C}})$ and gain accuracy Sampled noise on both C₁ and C₂ appear on output during ϕ_2



Capacitor sizing to meet noise requirements

For each stage: $P=[V_{SUP} \bullet GB \bullet C_{L}][V_{EB}]$

kT/C noise is contributed by each stage

If calibration is used to manage capacitor mismatch, capacitor sizing determined by noise requirements

Should capacitor area be allocated to put dominant noise on input stage or later stages?

If part of the total noise comes from latter stages, size of capacitors on input stage will be increased

Power Dissipation



Example: How do the op amp power requirements change from one-stage to the next with two bits per stage in a 16-bit pipeline. Assume a charge-redistribution gain stage and the size of the capacitors are scaled to keep the noise contributions the <u>same in each stage</u>. Assume the first stage has a total sampling capacitor of value C_1 and all noise is captured on input samples for each stage

Will keep the dc op amp gain for each stage the same

$$V_{n1} = \sqrt{\frac{kT}{C_1}}$$

$$V_{n2} = \sqrt{\frac{kT}{C_2}}$$

$$V_{n2} = 4V_{n1}$$

$$P_1 = X_F (14+1)C_{L1}$$

$$P_2 = X_F (12+1)\frac{1}{16}C_{L1} \cong 0.05 \bullet P_1$$

Power Dissipation



Example sol continued:

- $P = X_{i}(14+1)C_{i}$ $P_{2}=X_{F}(12+1)\frac{1}{16}C_{L1}$ $P_{3}=X_{F}(10+1)\frac{1}{16^{2}}C_{L1}$ $P_{4}=X_{F}(8+1)\frac{1}{16^{3}}C_{L1}$ $P_{s} = X_{F} (6+1) \frac{1}{16^{4}} C_{L1}$ $P_{_{6}}=X_{_{F}}(4+1)\frac{1}{16^{_{5}}}C_{_{L1}}$ $P_{T} = X_{F} (2+1) \frac{1}{16^{\circ}} C_{L1}$
- Power completely dominated by first stage
- Will likely not scale C so much so noise will be dominated by first stage
- No benefit from scaling power in latter stages

Pipelined Data Converter Design Guidelines

Issue

1. ADC offsets, Amp Offsets, Finite Op Amp Gain, DAC errors, Finite Gain Errors all cause amplifiers to saturate

2. Op Amp Gain causes finite gain errors and introduces noninearity

- 3. Op amp settling must can cause errors
- 4. Power dissipation strongly dependent upon GB of Op Amps

Strategy

- 1. Out-range protection circuitry will remove this problem and can make pipeline robust to these effects if α_k 's correctly interpreted
 - a) Use Extra Comparators
 - b) Use sub-radix structures
- 2. a) Select op amp architecture that has acceptable signal swing

b) Select gain large enough at boundary of range to minimize nonlinearity and gain errors

- 3. Select GB to meet settling requirements (degrade modestly to account for slewing)
- Minimize C_L, use energy efficient op amps, share or shut down op amp when not used, scale power in latter stages, eliminate input S/H if possible, interleave at high frequencies. Good (near optimal) noise ¹⁴ distribution strategy should be followed.

(technically tDC since TDC often refers to Temp to Digital Converter)



Both Pulse Width and Time Interval Requirements

(technically tDC since TDC often refers to Temp to Digital Converter)



Both Are Used

Applications:

Time of Flight (LIDAR, SONAR, RADAR)

Flow Meters

Chemical Reaction Times

Atomic collisions

Temperature Sensors

Alternative to Voltage Mode Data Conversion

Alternative to Voltage Mode Data Conversion

- Convert Analog Voltage to Pulse Width or Time Interval
- Use TDC to obtain Digital Output

Some argue that with decreasing supply voltage, voltage headroom is inherently limited but there is no fundamental limit in headroom or resolution when operating in the time domain

This is not the primary use of TDC today but is receiving some interest

One Basic Concept of a TDC



- Simple
- Modestly Accurate
- Slow

Another Basic Concept of a TDC



- Accurate
- Slow

Another Basic Concept of a TDC



- Accurate
- Slow



By appropriately setting delays in alternating two types of delay stages, pulse will disappear someplace in delay line

After pulse disappears, pulse width will be encoded in the thermometer code that appears in $\langle V_1, V_2, \dots, V_n \rangle$

Delay stages can be designed to shrink (or stretch) pulse by same amount in each stage

Very fine resolution in pulse shrink (or stretch) rate can be achieved by appropriate sizing of delay stages

If delay stages are programmable (discussed later) total delay can be accurately calibrated with ${\rm f}_{\rm REF}$

Large number of stages needed for high resolution

INL degrades with mismatch in delay elements

Vernier Delay Line Approach



Latch outputs determine how far input pulse propagated before arrival of t_B

Thermometer Code in Latch Outputs must be decoded

Large number of delay stages for high resolution

INL degrades with mismatch in delay elements

Resolution limited by delay of delay elements

Calibration with known time reference needed for reasonable accuracy

Dual Vernier Delay Line Approach



Delayed pulse in fast delay line "catches up" with pulse in slow line Arbiter determines which pulse arrives first Time difference thermometer coded in ARB outputs Very fine resolution is $\delta_A = \delta_B + \epsilon$ when ϵ is very small Useful for measuring very short pulses Number of stages gets large for high resolution Nonlinearity due to random variations in delay stages

Dual Vernier Delay Line Approach



Dual Vernier Delay Line Approach



One Arbiter Circuit

Pulse Shrinking TDCs





Odd number of inverting delay elements has received little attention (boring !)

But, it can be shown that if the delay elements are matched and a pulse is inserted into the loop, the pulse will circulate indefinitely !

Actually two or more pulses could circulate as well if there are a sufficient number of delay stages!

But even if the delay stages are ideally identical, random variations in delay characteristics will cause the a pulse to either stretch or shrink thus eventually causing the outputs to enter one of the two static Boolean states

Is there any practical use of this unique pulse-shrinking or pulse-stretching feature?

Pulse Shrinking TDCs



It can be shown that is a single delay element has different total propagation delays than the remaining elements, then a pulse inserted in the ring of an even number of inverting stages will stretch or shrink by precisely the same amount every time the pulse traverses the loop until it ultimately disappears and the stretch/shrink rate can be accurately controlled by judicious design of the delay stages.

Pulse Shrinking TDCs





Insert single "inhomogeneous" delay stage that causes pulse to shrink

Forms TDC with output in the Binary Counter after pulse disappears

Resolution can be very high by making difference between A and B delays very small

In contrast to Vernier approaches where random variations in delay cause INL errors, INL is very small since same elements are used for delay shrink each time pulse goes around loop



These structures have received minimal attention in the research community

Maybe they should be considered as a fundamental circuit structure that likely has a multitude of applications

Even some of the most basic properties of these structures have not been explored !

Gated Dual Vernier Delay Line TDC



Uses "gated" Ring Oscillators

Sampling array is an array of Arbiters

Claim high resolution is possible

Mismatch in delays introduce INL errors





Generic Inverting Delay State

- Input Port
- Output Port
- Load Port
- Program/Cal Port (optional)

Concept of Pulse Altering Circuit Applicable to Wide Array of Delay Stages





Some Reported Delay Cells





t_{SRK} is the amount of shrink for pulse looping once (independent of how often pulse loops)

$$t_{SRK} = T_{P1} - T_{P0} = t_{LH1} + t_{HL2} + t_{LH3} + \dots + t_{HLn} - t_{HL1} - t_{LH2} - t_{HL3} - \dots - t_{LHn}$$

Special Case 1 Even number of Identical Stages



$$t_{SRK} = T_{P1} - T_{P0} = t_{LH1} + t_{HL2} + t_{LH3} + \dots + t_{HLn} - t_{HL1} - t_{LH2} - t_{HL3} - \dots - t_{LHn}$$

Regrouping

$$t_{SRK} = t_{LH1} - t_{HL1} + t_{HL2} - t_{LH2} + t_{LH3} - t_{HL3} + \dots + t_{HLn} - t_{LHn}$$

If matched, t_{SRK}=0 so pulse circulated indefinitely

Special Case 2 Even number of with single mismatched on Stage 1

 $t_{\mbox{\scriptsize SRK}}$ is the amount of shrink for pulse looping once

 $t_{SRK} = T_{P1} - T_{P0} = t_{LH1} + t_{HL2} + t_{LH3} + \dots + t_{HLn} - t_{HL1} - t_{LH2} - t_{HL3} - \dots - t_{LHn}$

$$t_{SRK} = \delta_{LH1} + t_{LHN} + (-t_{HLN} - \delta_{HL1} + t_{HLN}) + (-t_{LHN} + t_{LHN}) + (-t_{HLN} + t_{HLN}) + (-t$$

This simplifies to

$$t_{SRK} = \delta_{LH1} - \delta_{HL1}.$$

pulse shrinks (if $t_{SRK} < 0$) or grows (if $t_{SRK} > 0$)

Special Case 3 Even number of with single mismatched on Stage 2

$$V_{P} \uparrow \sim T_{P0}$$

 $t_{\mbox{\scriptsize SRK}}$ is the amount of shrink for pulse looping once

 $t_{SRK} = T_{P1} - T_{P0} = t_{LH1} + t_{HL2} + t_{LH3} + \dots + t_{HLn} - t_{HL1} - t_{LH2} - t_{HL3} - \dots - t_{LHn}$

$$t_{SRK} = t_{LHN} + (-t_{HLN} + t_{HLN} + \delta_{HL2}) + (-t_{LHN} - \delta_{LH2} + t_{LHN}) + (-t_{HLN} + t_{HLN}) \dots (-t_{HLN} + t_{HLN}) - t_{LHN}$$

This simplifies to

$$t_{SRK} = \delta_{HL2} - \delta_{LH1}.$$

This is the negative of Special Case 2! So if pulse shrinks when in position 1 it will grow when in position 2

A new TDC based upon Pulse Shrinking Rings



Good INL since MSB determined by identical delay elements Vernier Delay Lines used to Enhance Resolution but Affect only LSB



Stay Safe and Stay Healthy !

End of Lecture 25